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In re application of : ARNE HUSTH
U.S. Serial No. : 09/923,242
Filed : August 3, 2001
For : DC COMPENSATION IN DIRECT CONVERSION RADIO
RECEIVERS
Group No. : 2631
Examiner : (Not Yet Assigned)

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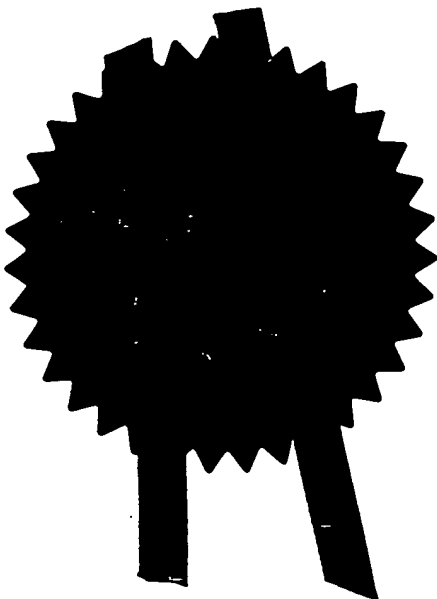
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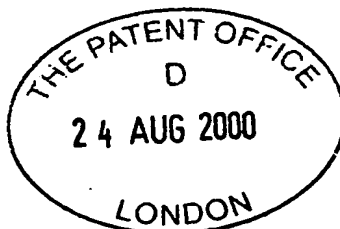


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Request for grant of a patent



1/77

The Patent Office

Cardiff Road
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Gwent NP9 1RH

1.	Your reference	03 36287		
2.	Patent application number	0020959.3		24 AUG 2000
3.	Full name, address and post code of the or each applicant	Nokia Mobile Phones Limited Keilalahdentie 4 02150 Espoo Finland		
	Patents ADP number	5911995004		
	If the applicant is a corporate body, give the country/state of its incorporation	FI		
4.	Title of the invention	DC COMPENSATION IN DIRECT CONVERSION RADIO RECEIVERS		
5.	Name of your agent	VENNER, SHIPLEY & CO		
	"Address for service" in the United Kingdom to which all correspondence should be sent	20 LITTLE BRITAIN LONDON EC1A 7DH		
	Patents ADP	1669004 ✓		
6.	If you are declaring priority from one or more earlier patent applications, give the country and the date of filing of the or each of these earlier applications and the or each application number	Country	Priority application number	Date of filing
7.	If this application is divided or otherwise derived from an earlier UK application, give the number and filing date of the earlier application	Number of earlier application		Date of Filing
8.	Is a statement of inventorship and of right to grant of a patent required in support of this request? (Answer 'YES' if: a) any applicant in 3. above is not an inventor, or b) there is an inventor who is not named as an applicant, or c) any named applicant is a corporate body)	YES		

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Description 11

Claim(s) 3

Abstract 1

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Statement of inventorship and right to grant of a patent (*Patents Form 7/77*)

Request for preliminary examination and search (*Patents Form 9/77*) 1

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11. I/We request the grant of a patent on the basis of this application.

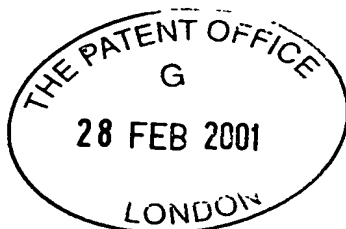
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Date

James Shiplin & Co.

24 August 2000

12. Name and daytime telephone number of person to contact in the United Kingdom JAN WALASKI
020 7600 4212



**Statement of inventorship and
of right to grant of a patent**

7/77

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Cardiff Road
Newport
Gwent NP9 1RH

1. Your reference 16 36287

2. Patent application number 0020959.3

3. Full name, address and post code of the or
each applicant Nokia Mobile Phones Limited
Keilalahdentie 4
02150 Espoo
Finland

Patents ADP number

If the applicant is a corporate body, give the
country/state of its incorporation FI

4. Title of the invention DC COMPENSATION IN DIRECT CONVERSION RADIO
RECEIVERS

5. State how the applicant(s) derived the right
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7. I/We believe that the persons named over the page (and on any extra
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020 7600 4212

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Enter  full names, addresses and postcodes of the inventors in the boxes and underline the surnames

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DUPLICATE

DC Compensation in Direct Conversion Radio Receivers

This invention relates to the field of direct conversion radio receivers, particularly but not exclusively to a method of DC compensation in a direct
5 conversion receiver.

Direct conversion radio receivers, also referred to as zero-IF receivers, inherently suffer from the problem of DC offsets. Sources of DC offset are present in all stages of a direct conversion receiver due to component
10 imbalances and tolerances. Further sources of DC offset include leakage of the local oscillator signal used in the receiver, for example, conduction and/or radiation of the local oscillator signal to the receiver antenna and leakage of the received signal into the local oscillator port of the RF mixers used in the receiver.

15 In a conventional direct conversion radio receiver operating, for example, in accordance with the GSM standard, which uses GMSK (Gaussian Minimum Shift Keying) modulation, the received signal is coupled to RF mixers which provide a baseband in-phase signal component I and a baseband quadrature
20 signal component Q.

A hardware solution to the DC offset problem is implemented in direct conversion receivers such as that used in the Nokia 6210™ mobile telephone. The fact that the receiver is intended for use with GSM time division multiple
25 access (TDMA) signals has been exploited to incorporate time periods in which the DC component of the I/Q signals can be clamped to zero by a DC cancellation (DCN) circuit. The timing of the DCN periods is controlled to occur in advance of the reception of any received signal burst. The DCN
circuits are designed as high pass filters, in which capacitors can be rapidly
30 charged/discharged during the DCN period by electronic switching circuits, to obtain a subtraction of the DC offset in each I or Q channel.

The weakness of this solution is that the precision of the DC compensation is dependent on the RF signal received during the DCN period. Because the DCN period lies in the time slot preceding the time slot allocated for the mobile station's own received signal, the signal in the DCN period can range from 0dBm to, for example, more than 30 dB higher than the level in the receive time slot allocated to the mobile station. When the received level in the DCN period is, for example, 30 dB higher than the mobile station's own received signal, the GMSK modulation cannot be averaged sufficiently by the DCN capacitors, resulting in an excessive residual DC content in the I/Q samples of the mobile station's own signal. This in turn results in a poor bit error rate (BER) for the received burst.

The above described problem also prevents direct conversion receivers using the DCN hardware solution from complying with certain tests used in GSM Type Approval, where signals which differ by 20dB between adjacent time slots are applied to a mobile station.

The present invention aims to address the above problems.

According to the present invention, there is provided a method of DC compensation for a direct conversion radio receiver, comprising the steps of determining the modulation extremes of a received modulated signal, determining a DC offset for the signal from the modulation extremes; and processing the signal to compensate for the offset.

The DC offset can be determined as substantially the mean of the signal amplitude at the modulation extremes. The modulation extremes can be determined from an inverse filtered signal, where the inverse filtering operation is applied to compensate for the response characteristic of the baseband circuit.

According to the present invention, there is further provided a direct conversion receiver comprising means for determining the modulation extremes of a received modulated signal, means for determining a DC offset for the signal from the modulation extremes; and means for processing the signal to
5 compensate for the offset.

According to the present invention, there is also provided a program to be executed by a digital signal processor in a direct conversion receiver, the receiver comprising a mixer circuit for providing quadrature related signals
10 from a received modulated signal, a dc cancellation circuit for cancelling the dc component in the quadrature related signals and a digital signal processor for removing a residual dc component from the signals, said program being configured to cause the digital signal processor to determine the modulation extremes of the signals, to calculate a dc offset for the signals from the
15 modulation extremes and to process the signals to compensate for the dc offset.

Embodiments of the invention will now be described, by way of example, with reference to the accompanying drawings, in which:

20 Figure 1 is a schematic block diagram illustrating a mobile telephone handset and its associated network;

Figure 2 is a schematic block diagram showing the mobile handset of Figure 1 in more detail;

Figure 3 is a block diagram of a direct conversion radio receiver which forms
25 the RF stage shown in Figure 2;

Figure 4 is a flow diagram illustrating the DC cancellation algorithm according to the invention;

Figure 5 shows a distorted I signal;

Figure 6 shows a filtered I signal;

30 Figure 7 shows the I signal after subtraction of a compensating exponential function from the sampled signal;

Figure 8a is a scattering diagram showing I/Q samples before applying compensation in accordance with the invention; and

Figure 8b is a scattering diagram showing the I/Q samples of Figure 8a after applying compensation in accordance with the invention.

5

In Figure 1, a mobile station in the form of a battery driven telephone cellular handset MS1, is shown schematically in radio communication with a public land mobile network PLMN 1.

10 The mobile handset MS1 includes a microphone 2, keypad 3, further keys comprising soft keys 4a, 4b and a navigation key 4c, a liquid crystal display 5, earpiece 6 and internal antenna 7. The handset 1 is WAP-enabled. The Nokia 6210™ is an example of a WAP-enabled mobile handset.

15 The circuitry of the handset 1 is shown in more detail in Figure 2. Signal processing is carried out under the control of a digital micro-controller 8 which has associated RAM 9 and flash memory 10. Electrical analogue audio signals are produced by microphone 2 and amplified by pre-amplifier 11. Similarly, analogue audio signals are fed to the earpiece 6 through an amplifier 12. The
20 micro-controller receives instruction signals from the keypad 3, soft keys 4a, 4b and navigation key 4c and controls operation of the LCD display 5. The soft-keys 4a, 4b comprise user-programmable keys, while the navigation key 4c comprises, for example, a roller device to perform a scrolling function for the display.

25

Information concerning the identity of the user is held on a smart card 13 in the form of a GSM SIM card which contains the usual GSM international mobile subscriber identity and encryption K_i that is used for encoding the radio transmission in a manner well known *per se*. The SIM card 13 is removably
30 received in a SIM card holder 14. Radio signals are transmitted and received by

means of the antenna 7 connected through an RF stage 15 to a codec 16 configured to process signals under the control of the micro-controller 8.

Thus, in use, for speech, the codec 16 receives analogue signals from the microphone amplifier 11, digitises them into a form suitable for transmission and feeds them to the RF stage 15 for transmission through antenna element 7 to the PLMN 1 shown in Figure 1. Similarly, signals received from the PLMN 1 are fed through the antenna element to be demodulated by the RF stage 15 and fed to codec 16 so as to produce analogue signals fed to amplifier 12 and earpiece 6.

Referring to Figure 3, the RF stage 15 includes a direct conversion receiver, which comprises a low noise amplifier (LNA) 20, which receives input signals from the antenna 7 and the output of which is connected to a mixer circuit 21 which comprises first and second mixers 22, 23, a local oscillator 24 and a 90° phase shifter 25. The output of the LNA 20 is connected to respective first inputs of the first and second mixers 22, 23. The output signal from the local oscillator 24 is connected to a second input of the first mixer 22 and, via the 90° phase shifter 25, to a second input of the second mixer 23. The respective outputs 26, 27 of the mixer circuit 21 are connected to a baseband circuit 28. The baseband circuit 28 comprises respective baseband amplifiers 29, 30, low pass filters 31, 32, DC cancellation circuits 33, 34 and analog-to-digital converters 35, 36. The respective outputs 37, 38 of the baseband circuit are fed to a digital signal processor 39.

25

The operation of the direct conversion receiver will now be described in detail. As mentioned above, GSM uses a modulation scheme known as Gaussian Minimum Shift Keying (GMSK). Reference is directed to Mouly & Pautet; "The GSM System for Mobile Communications", pages 249 to 259, for a detailed discussion of the GMSK modulation system for GSM. GMSK modulated signals are received at the antenna 7, amplified by the low noise

30

amplifier 20 and fed to the mixer circuit 21. The mixer circuit 21 uses the well-known technique of multiplying the modulated carrier with the local oscillator signal provided by the local oscillator 24 which has the same frequency as the carrier wave. The resulting outputs 26, 27 comprise a first signal 26 referred to as the in-phase channel I and a second signal 27 referred to as the quadrature channel Q. Taking the example of the I signal, this is amplified by a baseband amplifier 29 and filtered by a low pass filter 31. DC cancellation is then applied by a DC cancellation circuit (DCN) 33, and the resulting signal is digitised by the analog-to-digital converter 35 and fed to the DSP 39. The Q signal is processed in an exactly analogous way which is therefore not described separately. As mentioned previously, the DCN circuits 33, 34 are effectively high-pass filters, in which capacitors can be rapidly charged/discharged by electronic switching circuits during selected DCN periods, to obtain a subtraction of the DC offset in each of the I and Q channels. For example, during a DCN period, the received signal is used to rapidly charge a capacitor in the DCN circuit to a value which represents the DC content of the signal, so that the output of the DCN circuit during the following burst period, when the DCN function is deactivated, is compensated by the offset measured during the DCN period.

20

The I and Q samples received by the DSP 39 are still distorted by residual DC content as a result of insufficient DC cancellation in the DC cancellation circuits 33, 34. Additional DC compensation is therefore provided in the DSP software, which implements a DC cancellation algorithm, shown schematically in Figure 4.

25

A characteristic of GMSK modulation is that for a limited number N of I/Q samples, there is a sufficiently high probability that the I/Q vector has been positioned in all of the possible constellation points, or in other words that both the I and Q signals will have been in their modulation extremes. A modulation extreme results from a large number of successive repetitions of the

30

same symbol in the original NRZ (Non-Return-to-Zero) sequence to be transmitted. By finding the modulation extremes over N samples for each of the I and Q channels, the DC content can be calculated as the mean of the two extremes.

5

In the example described above, the receiver hardware is found to exhibit a high pass filter characteristic. As a result, the DC component in this example is a declining function; the DC content being largest at the start of the burst and zero at the end of the burst.

10

Figure 5 shows a distorted I signal from which the modulation extremes need to be determined. Referring to Figures 4 and 5, the signal is first filtered to straighten it, by applying an inverse filter to counteract the effect of the hardware high-pass filter characteristic (step s1).

15

Assuming that the high pass characteristics of the hardware can be modelled as a first order high-pass filter of the form:

20

$$H(s) = \frac{s}{s + 1/RC}$$

where RC denotes the effective RC product of the receiver circuit, then the inverse filter is implemented in the digital domain as:

25

$$S(z) = \frac{1 - \tau z^{-1}}{1 - z^{-1}}$$

where τ is a direct matched z - transform of the zero which cancels the single pole in $H(s)$, and

30

$$\tau = e^{-1/RC \cdot fs}$$

where f_s is the sample frequency.

The inverse filter is implemented in the DSP 39 as:

5

$$y = x - \tau xz^{-1} + yz^{-1}$$

The constant τ is tuned to a value representative of the components used in the direct conversion receiver hardware. With normal component tolerances, the value need only be determined once for each particular type of mobile station. For example, for the Nokia 6210™, the following values are used:

10

$$RC = 1.349 \times 10^{-4}, \tau = 0.973$$

15

Figure 6 shows the result of applying the inverse filter to the signal shown in Figure 5, at a sample rate which equals the symbol rate. In this example, only the first 64 samples in the burst are inverse filtered, as indicated by the window 40. 64 samples have been found to be a sufficiently high number to obtain the required probability of finding the modulation extremes. Although it is possible to scan a longer part of the burst to increase the chances of finding the true modulation extremes, such scanning requires a very accurate match of the inverse filter. If the match is not very accurate, a drift in the DC level can occur which increases for samples taken progressively further from the start of the burst.

20

25

The modulation extremes are then determined (step s2), being the signal amplitude values I_{\max} and I_{\min} within the 64 sample window 40 shown in Figure 6. The determined values are used to calculate the DC offset for the I channel (step s3):

30

$$I_offset = \frac{I_max + I_min}{2}$$

A similar procedure is carried out for the Q channel, resulting in a value of the offset for the Q channel (step s3):

$$Q_offset = \frac{Q_max + Q_min}{2}$$

As mentioned above, the high pass characteristics of the receiver hardware lead to the DC component in this example being a declining exponential function, so that compensation is performed by subtracting a weighted declining exponential function from the I/Q samples in the DSP, the algorithm providing an accurate determination of the initial DC content in the samples in the received burst and therefore the weighting for the exponential function.

The value of τ determined above is also used for the calculation of the declining exponential function used for compensation of the I/Q samples (step s4):

Exponential function:

$$E_n = E_{n-1} \cdot \tau$$

20

where $E_0 = 1$

Values to be subtracted from I samples: $IO_n = I_offset \cdot E_n$

The compensated I signals are determined by subtracting the weighted declining exponential function values from the original I samples (step s5):

$$I_{comp} = I_n - IO_n$$

Figure 7 shows the compensated I signal I_{comp} after subtraction of IO_n from the samples.

5 The Q signal is treated in an entirely analogous way to provide a compensated Q signal Q_{comp} .

Figure 8a is a scattering diagram of the I/Q samples without applying compensation in accordance with the invention. Figure 8b is a scattering diagram of the same samples after processing by the algorithm, illustrating the significant decrease in sample scattering observed in accordance with the invention.

15 In principle, it is also possible to subtract the determined DC offset values from the inverse filtered signal to obtain the final compensated I/Q signals, which can also enable the bandwidth reduction introduced by the hardware high-pass filter to be eliminated.

20 While the above example has been described in relation to a receiver having a first order high-pass characteristic, the receiver can have a baseband characteristic of a higher order. For such a receiver, a corresponding higher order inverse filter is applied in the DSP in order to straighten the signal to enable the modulation extremes to be determined.

25 Furthermore, for receivers which do not exhibit a high pass characteristic, there is a constant residual DC content in the signal received during the burst period. In this case, the inverse filtering operation is not required and compensation is achieved by subtracting a fixed DC level, rather than a declining exponential DC-level, from the received samples.

It will be appreciated that, once compensated I/Q values are available, subsequent processing is applied to correctly demodulate the GMSK signals and recover the original transmitted data, in a manner which is well known per se.

- 5 While the invention has been described in relation to GMSK modulation, the skilled person would appreciate that the principles could be applied to various other types of modulation, in particular constant amplitude modulation schemes, including for example the proposed 8PSK modulation scheme in the GSM EDGE evolution.

Claims

1. A method of DC compensation for a direct conversion radio receiver, comprising the steps of:
5 determining the modulation extremes of a received modulated signal;
determining a DC offset for the signal from the modulation extremes;
and
processing the signal to compensate for the offset.
- 10 2. A method according to claim 1, comprising determining the DC offset as substantially the mean of the signal amplitude at the modulation extremes.
3. A method according to claim 1 or 2, wherein the step of processing the signal comprises subtracting the offset from the signal.
- 15 4. A method according to claim 1 or 2, wherein the step of processing the signal comprises subtracting a weighted exponential function from the signal.
5. A method according to claim 4, wherein the weighting of the exponential
20 function comprises the determined DC offset.
6. A method according to any one of the preceding claims, wherein the receiver has an effective filter characteristic representing its frequency response, further comprising applying the inverse filter characteristic to the signal.
- 25 7. A method according to claim 6, including determining the modulation extremes from the inverse filtered signal.
8. A method according to any one of the preceding claims, wherein the
30 signal comprises an in-phase component of a modulated signal.

9. A method according to any one of the preceding claims, wherein the signal comprises a quadrature component Q of a modulated signal.

10. A method according to any one of the preceding claims, wherein the
5 signal is GMSK modulated.

11. A computer program which, when run on a processor, carries out the steps of any one of claims 1 to 10.

10 12. A direct conversion receiver comprising:
means for determining the modulation extremes of a received modulated signal;
means for determining a DC offset for the signal from the modulation extremes; and
15 means for processing the signal to compensate for the offset.

13. A receiver according to claim 12 having an effective filter characteristic representing its frequency response, further comprising inverse filter means to compensate for the filter characteristic.

20

14. A program to be executed by a digital signal processor in a direct conversion receiver, the receiver comprising a mixer circuit for providing quadrature related signals from a received modulated signal, a dc cancellation circuit for cancelling the dc component in the quadrature related signals and a
25 digital signal processor for removing a residual dc component from the signals, said program being configured to cause the digital signal processor to determine the modulation extremes of the signals, to calculate a dc offset for the signals from the modulation extremes and to process the signals to compensate for the dc offset.

30

15. A method of DC compensation for a direct conversion radio receiver substantially as hereinbefore described with reference to the accompanying drawings.

5 16. A direct conversion receiver substantially as hereinbefore described with reference to the accompanying drawings.

17. A program to be run on a digital signal processor substantially as hereinbefore described with reference to the accompanying drawings.

Abstract

DC Compensation for a Direct Conversion Radio Receiver

A direct conversion receiver uses an algorithm implemented by a DSP to cancel
5 residual dc offsets during demodulation of a GMSK modulated signal. The
algorithm exploits the characteristics of GMSK modulation by determining the
modulation extremes within sampled I/Q signals and calculates the DC offset as
the mean of the extremes. This offset is used to weight a declining exponential
function which is subtracted from the original signal samples to achieve
10 compensation.

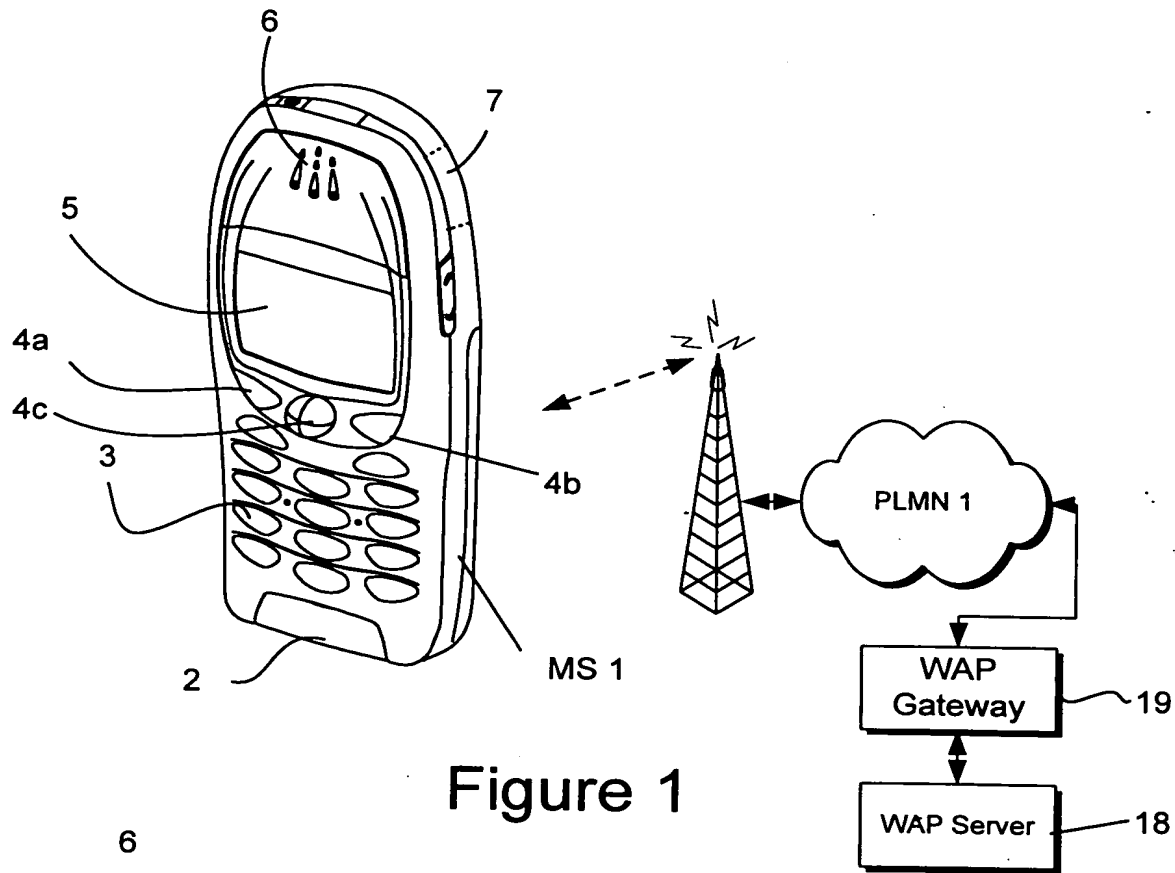


Figure 1

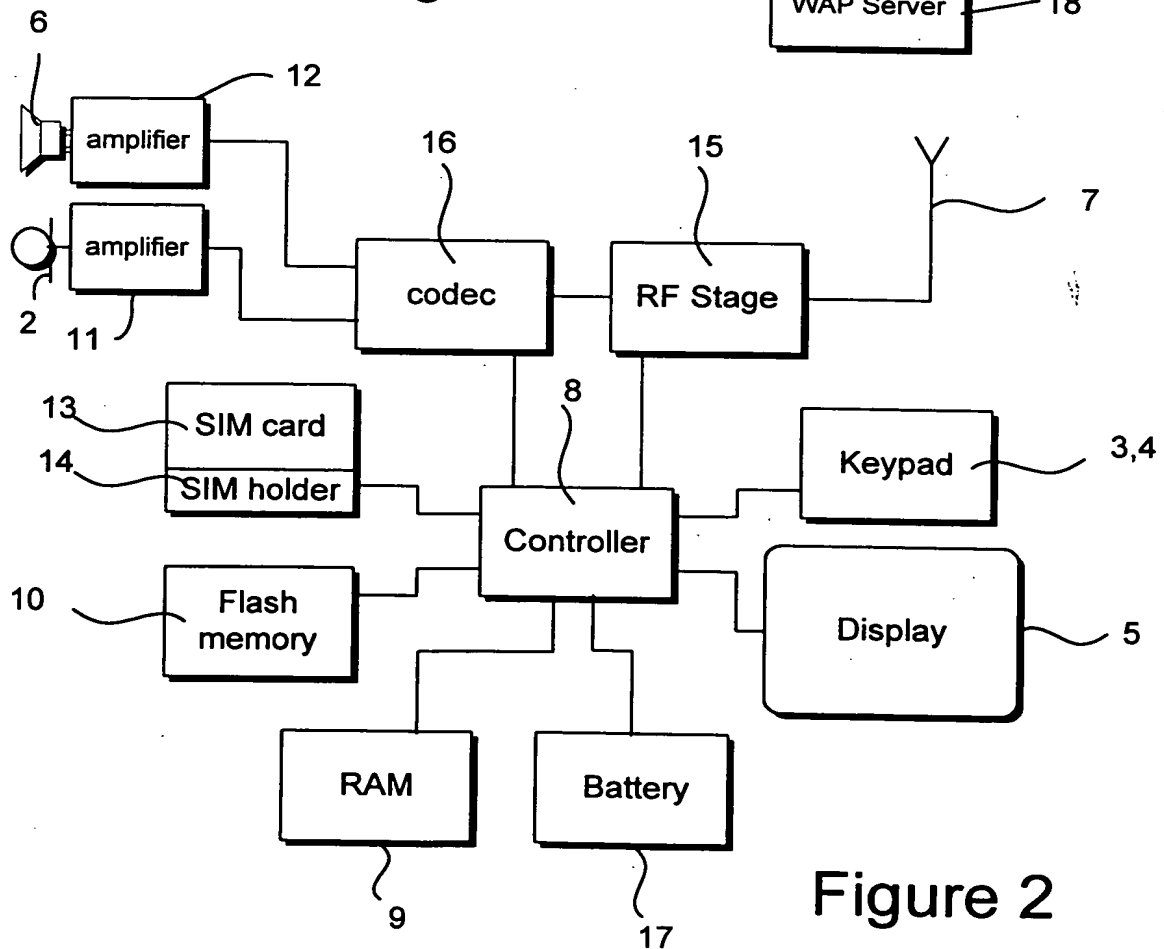


Figure 2

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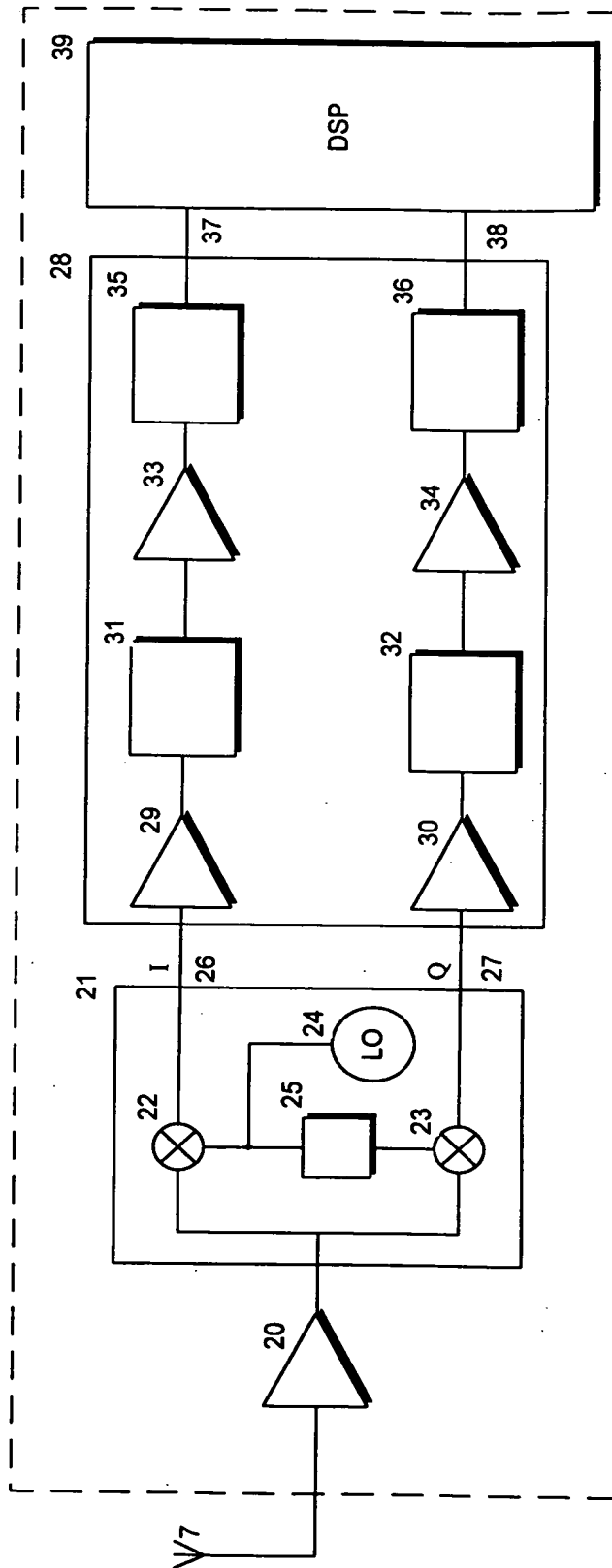


Figure 3

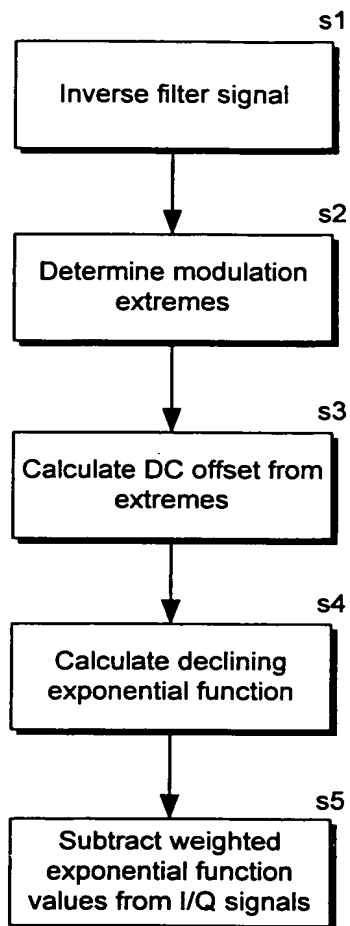


Figure 4

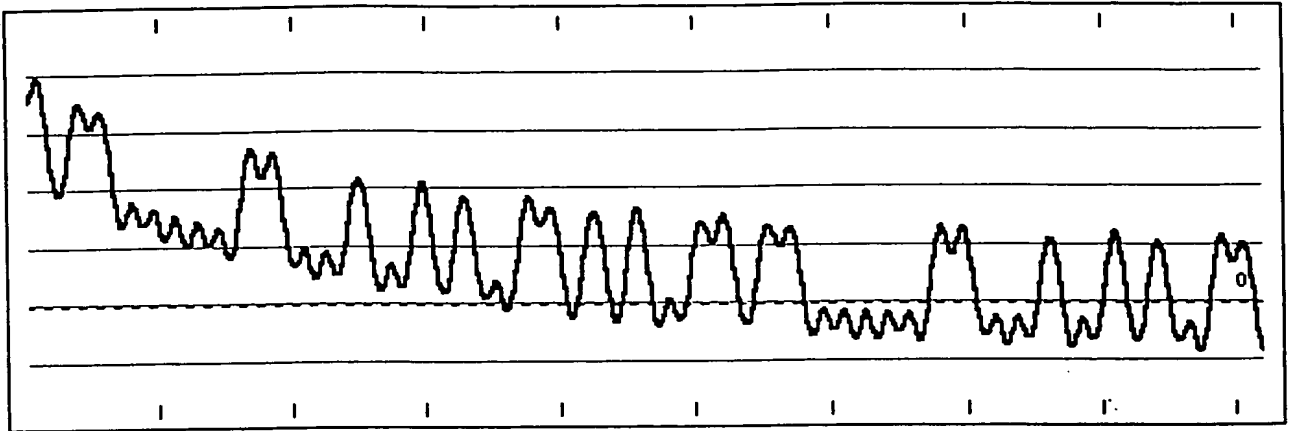


Figure 5

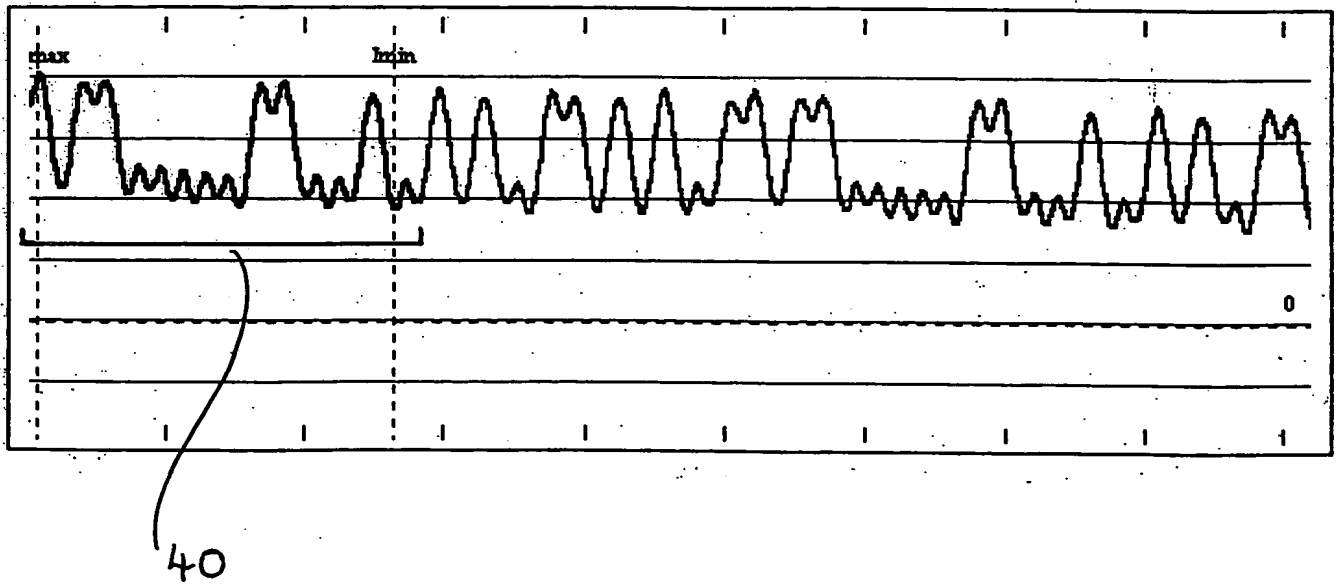


Figure 6

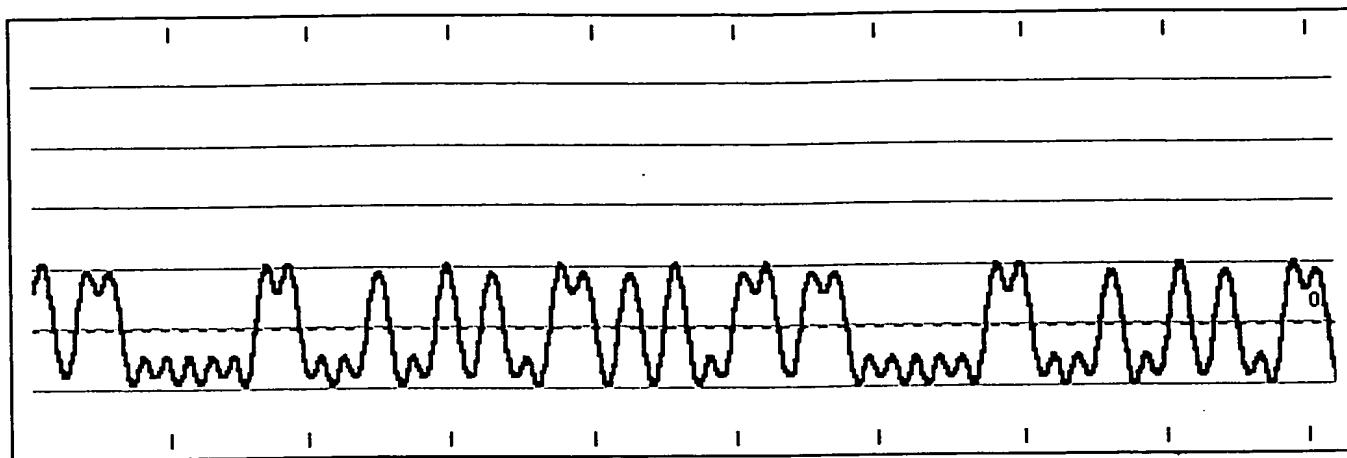


Figure 7

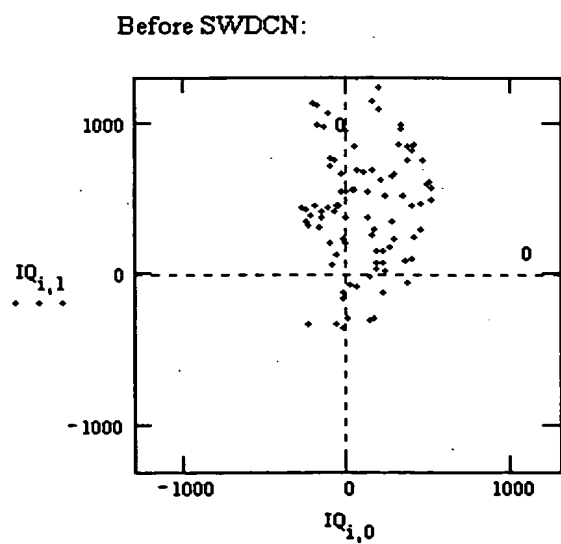


Figure 8a

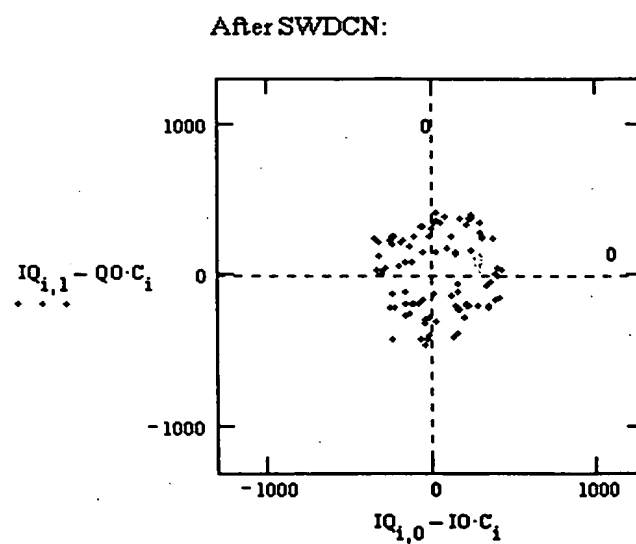


Figure 8b